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# SUSQUEHANNA RIVER BASIN

RACKET BROOK, LACKAWANNA COUNTY

PENNSYLVANIA

CARBONDALE NO. 4 DAM

National Dam Inspection Program.

PA-00384, DER ID Number 35-13), Susquehanna River Basin, Racket Brook, Lackawanna County, Pennsylvania.

Carbondale Number 4 Dam (NDI ID Number

CARBONDALE NO. 4 DAM Phase I Inspection Report.
NDI ID No. PA-00384 DER ID No. 35-13
PENNSYLVANIA GAS AND WATER COMPANY
15) DA CW 37-79-C-0075/
PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM
Prepared by (12) 83 p.
GANNETT FLEMING CORDDRY AND CARPENTER, INC. Consulting Engineers P.O. Box 1963 Harrisburg, Pennsylvania 17105
For
DEPARTMENT OF THE ARMY  Baltimore District, Corps of Engineers  Baltimore, Maryland 21203  FEBRUARY 1979
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#### PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

# SUSQUEHANNA RIVER BASIN

# RACKET BROOK, LACKAWANNA COUNTY

#### PENNSYLVANIA

# CARBONDALE\_NO. 4 DAM

NDI ID No. PA-00384 DER ID No. 35-13

#### PENNSYLVANIA GAS AND WATER COMPANY

# PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

#### FEBRUARY 1979

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#### PHASE I INSPECTION REPORT

#### NATIONAL DAM INSPECTION PROGRAM

#### BRIEF ASSESSMENT OF GENERAL CONDITION

#### AND

#### RECOMMENDED ACTION

Name of Dam: Carbondale No. 4

NDI ID No. PA-00384/DER ID No. 35-13

Owner: Pennsylvania Gas and Water Company

State Located: Pennsylvania

County Located: Lackawanna

ECONTO FROM

PP. 182]

W. Dr

Stream: Racket Brook

Date of Inspection: 25 October 1978

Inspection Team: Gannett Fleming Corddry and Carpenter, Inc.

Consulting Engineers

P.O. Box 1963

Harrisburg, Pennsylvania 17105

Based on visual inspection, available records, calculations and past operational performance, Carbondale No. 4 Dam is judged to be in good condition. The existing spillway can pass 59 percent of the Probable Maximum Flood (PMF) without overtopping of the dam. The spillway capacity is rated as inadequate. A stability analysis performed for this report indicates that the dam is apparently stable for the maximum loading condition.

The following measures are recommended to be undertaken by the Owner, in approximate order of priority, as soon as practical:

- (1) Raise the top of the dam to the design elevation.
- (2) Repair the concrete in the stilling basin and the mortar in the spillway weir masonry joints.

(3) Remove the brush from the embankment slopes and from the spillway discharge channel.

In addition, it is recommended that the Owner modify his operational procedures as follows:

- (1) Develop a detailed emergency operation and warning system for Carbondale No. 4 Dam.
- (2) Provide round-the-clock surveillance of Carbondale No. 4 Dam during periods of unusually heavy rains.
- (3) When warnings of a storm of major proportions are given by the National Weather Service, the Owner should activate his emergency operation and warning system procedures.

# Submitted by:

GANNETT FLEMING CORDDRY AND CARPENTER, INC.

Beltona

A. C. HOOKE Head, Dam Section

Date: 9 March 1979

Approved by:

DEPARTMENT OF THE ARMY BALTIMORE DISTRICT, CORPS OF ENGINEERS

PROFESSIONAL

ALBERT CHARLES HOOK

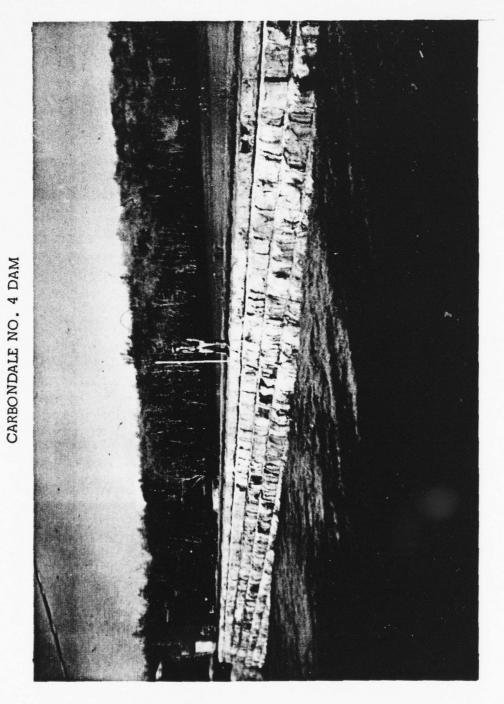
ENGINEER

G. K. WITHERS

Colonel, Corps of Engineers

District Engineer

DATE: 21 Mar 79



#### SUSQUEHANNA RIVER BASIN

#### RACKET BROOK, LACKAWANNA COUNTY

#### PENNSYLVANIA

#### CARBONDALE NO. 4 DAM

NDI ID No. PA-00384 DER ID No. 35-13 PENNSYLVANIA GAS AND WATER COMPANY

PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM

#### SECTION 1

#### PROJECT INFORMATION

#### 1.1 General.

- a. Authority. The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.
- b. <u>Purpose</u>. The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

# 1.2 Description of Project.

a. Dam and Appurtenances. Carbondale No. 4 Dam is a masonry dam with earthfill to the top of the dam along the upstream face and earthfill to within 3 to 10 feet of the top of the dam along the downstream face. The dam extends about 580 feet across the valley and is 28 feet high at maximum section, The spillway, an integral part of the masonry dam, is located near the right abutment. It has

a rounded crest, and the crest length is 100 feet. The spillway crest is 4.0 feet below the design elevation of the top of the dam. Immediately below the spillway is a concrete stilling basin with baffle blocks. At the end of the stilling basin is a riprapped channel, which extends a short distance to the natural stream. There are dams both upstream and downstream of Carbondale No. 4 Dam as noted below. The various features of Carbondale No. 4 Dam are shown on the Plates at the end of the report and on the Photographs in Appendix D.

- b. Location. The dam is located on Racket Brook approximately 2.0 miles east of Carbondale, Pennsylvania. Carbondale No. 4 Dam is shown on USGS Quadrangle, Waymart, Pennsylvania, with coordinates N41 34 '30" W75 27 '35", in Lackawanna County, Pennsylvania. The Wayne County Line is at the east end of the dam. Most of the reservoir is in Wayne County. The dam is 0.7 mile upstream of Brownell Dam. Carbondale No. 4 Dam is also 0.6 mile downstream of Carbondale No. 7 Dam. Both Brownell Dam and Carbondale No. 7 Dam are are on Racket Brook. The location map is shown on Plate 1.
- c. <u>Size Classification</u>. Intermediate (28 feet high, 1,071 acre-feet).
- d. <u>Hazard Classification</u>. High hazard. Downstream conditions indicate that a high hazard classification is warranted for Carbondale No. 4 Dam (Paragraph 5.1c.).
- e. Ownership. Pennsylvania Gas and Water Company, Wilkes-Barre, Pennsylvania.
- f. Purpose of Dam. Water supply for Carbondale, Pennsylvania and surrounding communities.
- g. Design and Construction History. Carbondale No. 4
  Dam was built in 1892 for the Crystal Lake Water Company.
  The dam was designed by E. Sherman Gould, consulting engineer of Scranton. The construction was supervised by George A.
  Wright. The contractor was Babcock and Kelley of Unadilla,
  New York.

During the flood of June, 1942 the dam was overtopped by a small amount. No damage to the dam was reported but a road immediately downstream was washed out. In 1945, the original spillway at the left abutment was filled in and the present spillway at the right abutment was constructed.

At the same time, the present stilling basin was constructed, the outlet works pipe was extended, modifications were made to the downstream earthfill, a dry masonry wall was added along the left side of the spillway approach channel, and riprap was added along the right side of the approach channel. The modification was designed by H.A. Vicker, the Owner's Chief Engineer, and built by Harrison and Byron, Contractors of Jersey City, New Jersey.

h. <u>Normal Operational Procedure</u>. The reservoir is normally maintained at spillway crest level. The valve on the outlet conduit is normally closed.

# 1.3 Pertinent Data.

a.	Drainage Area. (square miles)	1.7
b.	Discharge at Damsite. (cfs.) Maximum known flood at damsite  Outlet works at maximum pool elevation  Spillway capacity at maximum pool elevation  Design spillway capacity	700 70 2,400 2,930
c.	Elevation. (Feet above msl.) Top of dam (low area) Design top of dam Maximum pool (top of dam low area) Normal pool (spillway crest) Upstream invert outlet works - not available Downstream invert outlet works Streambed at downstream toe of dam (2)	1745.2 1745.7 1745.2 1741.7  1717.0 1716.0
d.	Reservoir Length. (Miles.) Normal pool Maximum pool	. 44
e.	Storage. (Acre-feet.) Normal pool Maximum pool (design)	810 1,071
f.	Reservoir Surface. (Acres.) Normal pool Maximum pool (design)	62 68

<sup>(1)</sup> See Section 5 for discussion of the maximum known flood.

<sup>(2)</sup> Approximate.

g. Dam. Type -

> Length - Feet. Height - Feet (design). Top width - Earthfill (minimum) - Feet Masonry - Feet

Side slopes -

Impervious core -Zoning -Cutoff -

Grout curtain -

- Diversion and Regulating Tunnel. h.
- i. Spillway. Type -

Length of weir - Feet Crest elevation Upstream channel -

Downstream channel -

Regulating Outlets j.

Masonry with earthfill to full height upstream and to partial height downstream.

480 28 12

Downstream 3V on 1H (Masonry) Upstream-Varies 1V on 2.25H to 1V on 5H. Masonry None in earthfill. Masonry founded on bed-

None.

None.

Masonry weir with rounded crest. 100 1741.7 Mild slope to

reservoir. Stilling basin and short reach of riprapped channel.

One 24-inch diameter cast iron pipe which transitions to a 36inch diameter pipe downstream of the masonry section. Two 24-inch gate valves, in series, are provided upstream of the masonry section.

#### ENGINEERING DATA

# 2.1 Design.

- a. Data Available. Very little engineering data were available for review for the original structures. In a study performed in 1914 by the Pennsylvania Water Supply Commission, an account of design concepts, geology, construction materials and methods, and design features was prepared from interviews with the Owner, visual inspection, and other sources. The 1914 study also included analyses for hydrology and hydraulics as well as an analysis of the structural stability. A summary of the results of the analyses are on file. The construction specifications for the 1945 modification are on file. A design analysis for the 1945 modification that is available for review includes both hydraulic and structural data.
- b. Design Features. The dam and appurtenances are described in Paragraph 1.2a. The design features are shown on the Plates at the end of the report and on the Photographs in Appendix D. Plate 2 shows a plan of the dam. Plate 3 and Photographs A and B show the profile and a section of the masonry. This plate was drawn before the 1945 modifications to the dam and it shows the original spillway at the left abutment. Plate 4 and Photographs C, D, and E show a profile of the existing spillway and outlet works. The outlet works pipe is extended further, as shown on Plate 2. The extension is noted as a 30-inch diameter pipe; the extension is actually 36-inches in diameter. The other pipe, parallel to the outlet works pipe on Plate 2, apparently connects to a drain from the valve house.
- c. <u>Design Considerations</u>. The information available for review did not raise any concerns about the original design, except for the spillway capacity. This has subsequently been modified.

#### 2.2 Construction.

a. <u>Data Available</u>. Construction data available for review for the original structures was limited to information contained in the 1914 report prepared by the Pennsylvania Water Supply Commission. That information was obtained by interviews with the Owner, and it gives details of the construction operations.

- b. Construction Considerations. The 1914 report praises the quality of construction used in the structure. For example, information is cited that indicates that only the best cement was used, that the contractor was very experienced in this type of construction, and that the specifications were rigidly enforced. The accounts of construction are such that it appears reasonable care was used in construction of Carbondale No. 4 Dam. Review of the available information for the 1945 improvements did not yield pertinent information with respect to the character of that work.
- 2.3 Operation. There are no formal records of operation. As noted herein, the dam was overtopped in 1942. The spillway was subsequently modified in 1945. Based on information from the Owner and the caretaker of the dam, all structures have performed satisfactorily since the 1945 modification.

# 2.4 Evaluation.

- a. Availability. Engineering data was provided by the Division of Dams and Encroachments, Bureau of Water Quality Management, Department of Environmental Resources, Commonwealth of Pennsylvania (PennDER), and by the Owner, Pennsylvania Gas and Water Company. The Owner made available a senior construction supervisor for information during the visual inspection. The Owner also researched his files for additional information upon request of the inspection team.
- b. Adequacy. The type and amount of design data and other engineering data is limited, and the assessment must be based on the combination of available data, visual inspection, performance history, hydrologic assumptions, and hydraulic assumptions.
- c. Validity. There is no reason to question the validity of the available data.

#### VISUAL INSPECTION

# 3.1 Findings

- a. General. The overall appearance of the dam was good, with some deficiencies as noted herein. The locations of some of these deficiencies are shown in Appendix B on Plate B-1. Survey data acquired during this inspection is presented in Appendix B. On the day of the inspection, the pool was at spillway crest elevation.
- b. Composite Masonry Gravity and Earthfill Section. This section is in good condition. No deficiencies were noted on the masonry. The top of the section is at or above the design elevation except at the right abutment, where the top is 0.5 foot below the design elevation. This area is an abandoned railroad bed (Photograph E). The mortar in the masonry joints is in good condition. The earthfill downstream of the masonry is in good condition. It is very flat and well maintained (Photograph B). The embankment upstream of the masonry is in good condition (Photograph A). The riprap on the upstream slope appeared to be in good condition. There is a minor amount of brush on the upstream slope. The survey performed for this inspection revealed that the upstream earthfill slope varies, with the steepest section being 1V on 2.25H.
- c. Appurtenant Structures. The outlet works is in good condition. Two men opened the 24-inch valve about 5 percent in 5 minutes with no problems noted. On the day of inspection, the inlet was submerged. The pipe discharges directly into the stream about 200 feet downstream from the masonry section. The stream at the outfall is slightly overgrown with brush and trees. Seepage of about 0.5 gpm was observed in the stream.

The spillway is in fair condition. There is a flow of about 1 gpm seeping from a joint located a few inches below the crest. There is seepage from many other joints. The seepage is from both the joints in the spillway and those immediately to the right of the spillway (Photograph C).

There are many deficiencies in the stilling basin (Photograph D). One baffle block is badly spalled. Pattern cracking and leaching were observed at the right wall. The right wall is badly spalled in many areas. The reinforcing bars are exposed along the top of this wall. There is also some spalling at the left wall near its junction with the spillway. About 80 percent of the bottom of the stilling basin is scoured. In some areas, the concrete appears to have scoured completely. A total flow of 2 gpm was observed in the stilling basin. It was not possible to determine whether this flow was seeping from beneath the stilling basin or whether it was the accumulated seepage from the spillway joints.

The riprapped channel downstream from the stilling basin is heavily overgrown with brush and small trees (Photograph D).

- d. Reservoir Area. The reservoir has generally gentle slopes. The watershed is mostly uninhabited and undeveloped. Some of it is owned and controlled by Pennsylvania Gas and Water Company. The remainder is mostly owned and controlled by the Commonwealth. Carbondale No. 7 Dam upstream is used by Farview State Hospital for water supply. A brief visit was made to Carbondale No. 7 Dam on the day of the inspection (Photograph F).
- e. <u>Downstream Channel</u>. Downstream from the rip-rapped channel, the natural channel proceeds for a short distance to a 60-inch diameter culvert passing under U.S. Route 6. The roadway embankment is 10 feet high at this crossing. The stream flows for 0.7 mile through an uninhabited and wooded reach to Brownell Reservoir. Access to the dam is from U.S. Route 6, which passes very close to the left abutment.

#### OPERATIONAL PROCEDURES

- 4.1 Procedure. The reservoir is maintained at spill-way crest, Elevation 1741.7, with excess inflow discharging over the spillway and into Racket Brook, which flows into Brownell Reservoir 0.7 mile downstream. A 24-inch diameter cast-iron pipe discharges water from the reservoir. Streamflows in Racket Brook can be increased by releases from Carbondale No. 4 Dam. Since streamflow is usually augmented only when Brownell Reservoir is below spillway crest elevation, the valve on the Carbondale No. 4 water discharge line is usually closed.
- 4.2 Maintenance of Dam. The dam is visited daily by a caretaker who records the reservoir elevation. Weekly reports are mailed to the Owner's Engineering Department. This information is used by the Owner's Engineering Department for regulating flows in the distribution system. The caretaker is also responsible for observing the general condition of the dam and appurtenant structures and for reporting any changes or deficiencies to the Owner's Engineering Department. A Pennsylvania Gas and Water Company engineer makes a formal inspection of the dam each year, and the records are filed and used for determining priority of repairs. Informal inspections are also made when the engineer is on the site for other reasons. The grass is mowed frequently. Brush on the upstream embankment is cut on a regular basis.
- 4.3 Maintenance of Operating Facilities. The valve on the outlet works pipe is operated annually. In response to the Phase I Dam Inspection Program of the previous year, the Owner is revising his maintenance procedures. Details of the procedures are still being developed.
- 4.4 Warning Systems in Effect. The Owner furnished the inspection team with a verbal description of the chain of command for Carbondale No. 4 Dam and of a generalized emergency notification list that is applicable for all of the Pennsylvania Gas and Water Company dams. The Owner said that during periods of heavy rainfall, available personnel are dispatched to the dams to observe conditions.

All company vehicles are equipped with radios, and the personnel can communicate with each other and with a central control facility. Evaluation of risk is made by the Owner's Engineering Department. The Owner's Engineering Department is also responsible for notification of emergency conditions to the local authorities. Detailed emergency operational procedures have not been formally established for Carbondale No. 4 Dam, but are as directed by the Owner's Engineering Department.

4.5 Evaluation of Operational Adequacy. Maintenance of the dam, except for the brush in the spillway outlet channel, appears good. The maintenance procedures for the outlet works valve appear good. The procedures used by the Owner for inspecting the dam are adequate, but some needed repairs have not been made. In general, the warning system is adequate, but it would be more effective if it were more detailed.

#### HYDRAULICS AND HYDROLOGY

# 5.1 Evaluation of Features.

- a. Design Data. In the report upon the application of the Owner to modify the dam in 1945, the Pennsylvania Power Commission estimated the design spillway capacity at 2,930 cfs. Computations made for this report show that this estimate was reasonable, and it was used for this report.
- b. Experience Data. The Owner has not reported any hydraulic problems with the dam since the 1945 modifications. The dam was overtopped by a small amount in 1942. The spillway prior to 1945 had a discharge capacity of 200 cfs. The height of overtopping was not reported. Assuming that the dam overtopped by 0.5 foot, the resultant outflow computes to be about 700 cfs. This is used as the flood of record.

# c. Visual Observations.

- (1) General. The visual inspection of Carbondale No. 4 Dam, which is described in Section 3, resulted in a number of observations relevant to hydraulics and hydrology. These observations are evaluated herein for the various features.
- (2) Embankment. The low area at the right abutment reduces the spillway discharge capacity. In all probability, when the railroad track was removed, the railroad fill was graded to below the top elevation of the dam.
- (3) Appurtenant Structures. Although the outlet works pipe extends under pressure through the earthfill, it also extends through the masonry section. The valve is upstream of the masonry section. The closure facilities for the outlet works pipes are adequate.

The brush in the spillway outlet channel will reduce its carrying capacity. The backwater effect will not reduce the spillway discharge capacity. However, it may cause overtopping of the stilling basin

walls. If the walls should overtop, erosion of the downstream earthfill would occur. Although undesirable, it would not create a significant hazard to the embankment.

- (4) Reservoir Area. No conditions were observed in the reservoir area or watershed that might present significant hazard to the dam. Pertinent data for Carbondale No. 7 Dam, located 0.6 mile upstream from Carbondale No. 4 Dam, is listed in Appendix C. The assessment of the dam is based on existing conditions, and the effects of future development are not considered.
- (5) Downstream Conditions. No conditions were observed immediately downstream of the dam that would create significant hazard to the dam. If the dam should fail, a hazard to U.S. Route 6 would exist. In addition, the floodflows would discharge into Brownell Reservoir. A Phase I Inspection Report for the National Dam Inspection Program has previously been prepared for Brownell Dam, which is of intermediate size. Brownell Dam was classified as high hazard, with a seriously inadequate spillway. As the failure of Carbondale No. 4 Dam could cause the overtopping of Brownell Dam, a high hazard classification is warranted for Carbondale No. 4 Dam. Access to Carbondale No. 4 Dam is good.

# d. Overtopping Potential.

- (1) Spillway Design Flood. According to the criteria established by the Office of the Chief of Engineers (OCE) for the size (Intermediate) and hazard potential (High) of Carbondale No. 4 Dam, the spillway design flood (SDF) is the probable maximum flood (PMF).
- (2) Description of Model. The watershed was modeled with the HEC-1DB computer program. The HEC-1DB computer program computes a PMF runoff hydrograph and routes the flows through both reservoirs and stream sections. In addition, it has the capability to simulate an overtopping dam failure. The PMF inflow component to Carbondale No. 7 Reservoir was determined and routed through the dam. The outflow from the dam was routed, downstream to Carbondale No. 4 Reservoir and added to the uncontrolled runoff occurring upstream of Carbondale No. 4 Dam. The combined runoff was routed through Carbondale No. 4 Dam. Identical methods were used for various percentages of the PMF.

(3) Summary of Results. Pertinent results are tabularized at the end of Appendix C. The analysis reveals that Carbondale No. 7 Dam can pass about 66 percent of its component of the PMF without overtopping. Carbondale No. 4 Dam, with its existing top elevation of 1745.2 can pass approximately 59 percent of the PMF without overtopping.

If the Carbondale No. 4 Dam were raised to its design elevation of 1745.7, it would be able to pass approximately 72 percent of the PMF.

(4) Spillway Adequacy. The criteria used to rate the spillway adequacy of a dam are described in Appendix C. Since Carbondale No. 4 Dam cannot pass the PMF but can pass the 1/2 PMF, the spillway capacity is rated as inadequate. If the dam were raised to its design elevation, the spillway would still be rated as inadequate.

#### STRUCTURAL STABILITY

# 6.1 Evaluation of Structural Stability.

#### a. Visual Observations.

- (1) General. The visual inspection of Carbondale No. 4 Dam, which is described in Section 3, resulted in a number of observations relevant to structural stability. These observations are evaluated herein for various features.
- (2) Embankment. Trees and brush growing on the embankment are undesirable. The low area of the embankment is evaluated in Section 5.
- (3) Appurtenant Structures. No deficiencies relevant to structural stability were observed at the outlet works. The seepage near the outlet works is not excessive. It probably does not originate at the dam. The conditions observed at the spillway and stilling basin are caused by a lack of maintenance.
- b. Design and Construction Data. In the 1914 report by the Pennsylvania Water Supply Commission, the stability of the masonry gravity section was analyzed. The analysis was based on the following assumptions: the pool at the top of the dam, no tailwater, uplift of two-thirds the full hydrostatic pressure at the heel, and that soil pressure on the upstream face could be neglected. The resultant was within the middle third for all sections, with adequate toe pressures and factors of safety against sliding.

A stability analysis for the masonry gravity section was performed in this study. Only the bottom section was considered. The loading assumptions are as follows: reservoir level at the top of the dam, full hydrostatic pressure and at-rest earth pressure on the upstream face, uplift varying uniformly from full tailwater at the toe to full tailwater at the heel plus two-thirds of the difference between the headwater and tailwater also at the heel, and no passive earth pressure on the downstream face.

The results of the stability analysis show that the toe pressure and sliding factor are within acceptable limits and that the resultant is within the middle third, about 9.9 feet from the toe. OCE guideline on overturning recommends that the resultant be within the middle third. The structure is apparently stable for this loading condition.

- c. Operating Records. There are no formal records of operation. According to the Owner, no stability problems have occurred over the operational history of the dam.
- d. Postconstruction Changes. The 1945 modification to the spillway was accomplished by removing the upper 6 feet of the masonry gravity section and then constructing a 2-foot high cap on the section. The net reduction in height is 4 feet. Using simplifying assumptions, calculations indicate that the resultant is still within the middle third and both the factor of safety against sliding and the toe pressure are within acceptable limits.
- e. <u>Seismic Stability</u>. Carbondale No. 4 Dam is located in <u>Seismic Zone 1</u>. Normally it can be considered that if a dam in this zone has adequate factors of safety under static loading conditions, it can be assumed safe for any expected earthquake loading. However, since there is the possibility of earthquake forces cracking the masonry gravity section, the theoretical seismic stability of Carbondale No. 4 Dam cannot be assessed.

# ASSESSMENT, RECOMMENDATIONS, AND

#### PROPOSED REMEDIAL MEASURES.

# 7.1 Dam Assessment.

# a. Safety.

- (1) Based on visual inspection, available records, calculations, and past operational performance, Carbondale No. 4 Dam is judged to be in good condition. With existing conditions, the spillway can pass 59 percent of the PMF without overtopping of the dam. The spillway capacity is rated as inadequate. If the Dam were raised to its design elevation, it could pass 72 percent of the PMF. The spillway capacity would still be rated as inadequate.
- (2) A stability analysis for the dam was performed for this report. This was accomplished using some assumed values. For the loading condition considered, the resultant is within the middle third of the base and both the toe pressure and factor of safety against sliding are within acceptable limits.
- (3) The visual inspection resulted in some deficiencies, which are summarized below for the various features.

#### Feature and Location

Embankment:

Upstream slope

Top

Spillway:

Stilling Basin

Downstream channel

Observed Deficiency

Trees and brush Below design elevation

Deteriorated mortar Spalling, pattern cracking, scour, and leaching. Brush

- b. Adequacy of Information. The information available is such that an assessment of the condition of the dam can be inferred from the combination of visual inspection, past performance, and computations performed prior to and as part of this study.
- c. <u>Urgency</u>. The recommendations in Paragraph 7.2 should be implemented as soon as practical.
- d. Necessity for Further Investigations. In order to accomplish some of the remedial measures outlined in Paragraph 7.2, further investigations by the Owner will not be required.

# 7.2 Recommendations and Remedial Measures.

- a. The following measures are recommended to be undertaken by the Owner, in approximate order of priority, as soon as practical:
- (1) Raise the top of the dam to the design elevation.
- (2) Repair the concrete in the stilling basin and the mortar in the spillway weir masonry joints.
- (3) Remove the brush from the embankment slopes and from the spillway discharge channel.
- b. In addition, it is recommended that the Owner modify his operational procedures as follows:
- (1) Develop a detailed emergency operation and warning system for Carbondale No. 4 Dam.
- (2) Provide round-the-clock surveillance of Carbondale No. 4 Dam during periods of unusually heavy rains.
- (3) When warnings of a storm of major proportions are given by the National Weather Service, the Owner should activate his emergency operation and warning system procedures.

# SUSQUEHANNA RIVER BASIN RACKET BROOK, LACKAWANNA COUNTY PENNSYLVANIA

CARBONDALE NO. 4 DAM

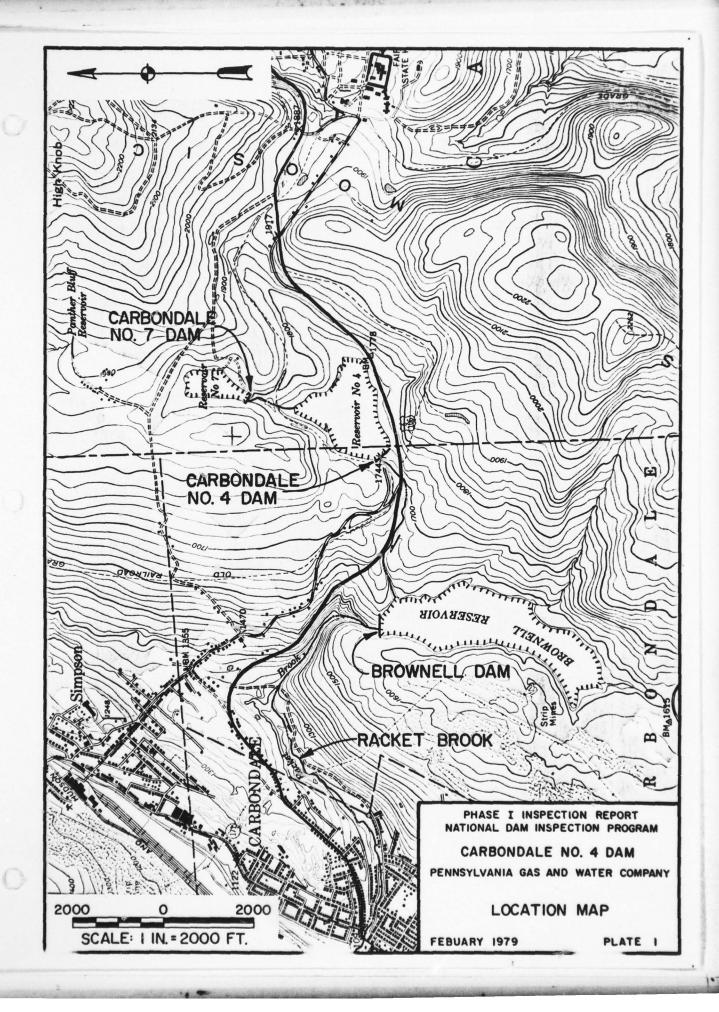
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PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM

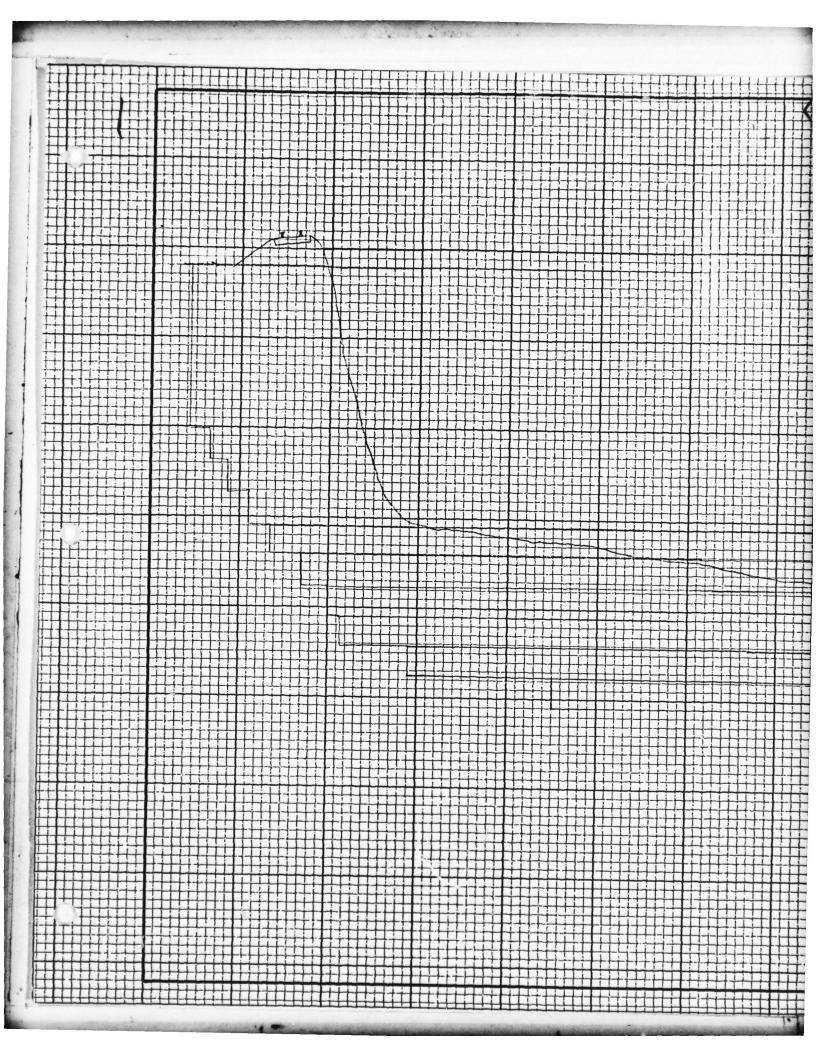
FEBRUARY 1979

**PLATES** 



RESERVOIR INTAKE CHAMBER TOP OF DAM 1745.7 SOILLNAY FLUN CLINER 1741.63 CONCRETE APRON . Branch Splitter Piers Bed Jed Co pour dent Good . 6.6 110 De l'or con l'angle CARBONO ALE NO.4DAM
Spillway & Channel as
Reconstructed in 1945
Scale: Ilach = 50 Feet

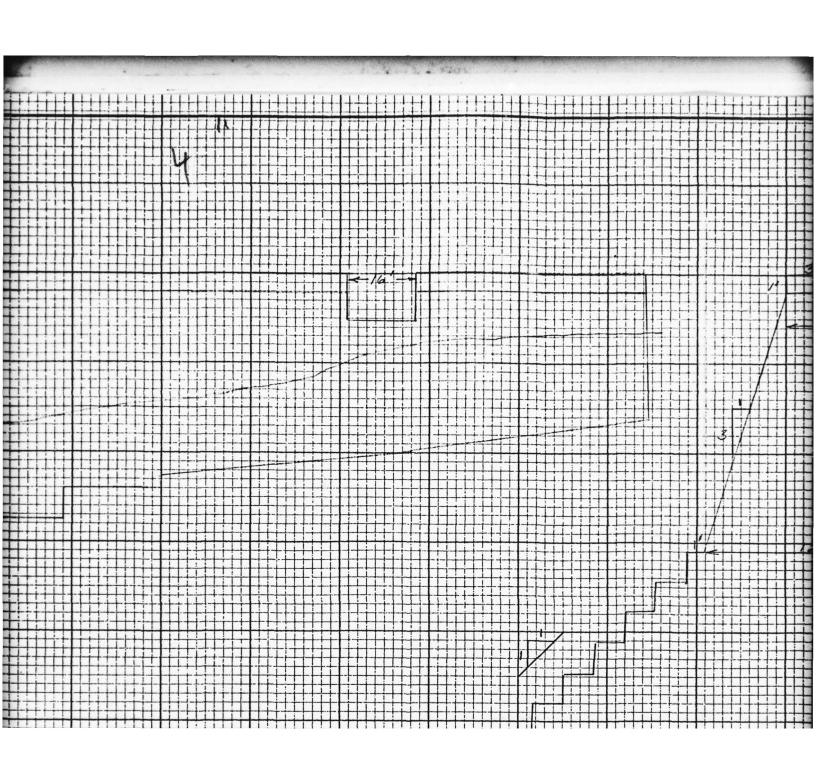
RVOIR TOP OF DAM 17457 To Honesdale Poute No. Blow-off Channel To Carbondele PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM CARBONDALE NO. 4 DAM PENNSYLVANIA GAS AND WATER COMPANY PLAN FEBUARY 1979 PLATE 2

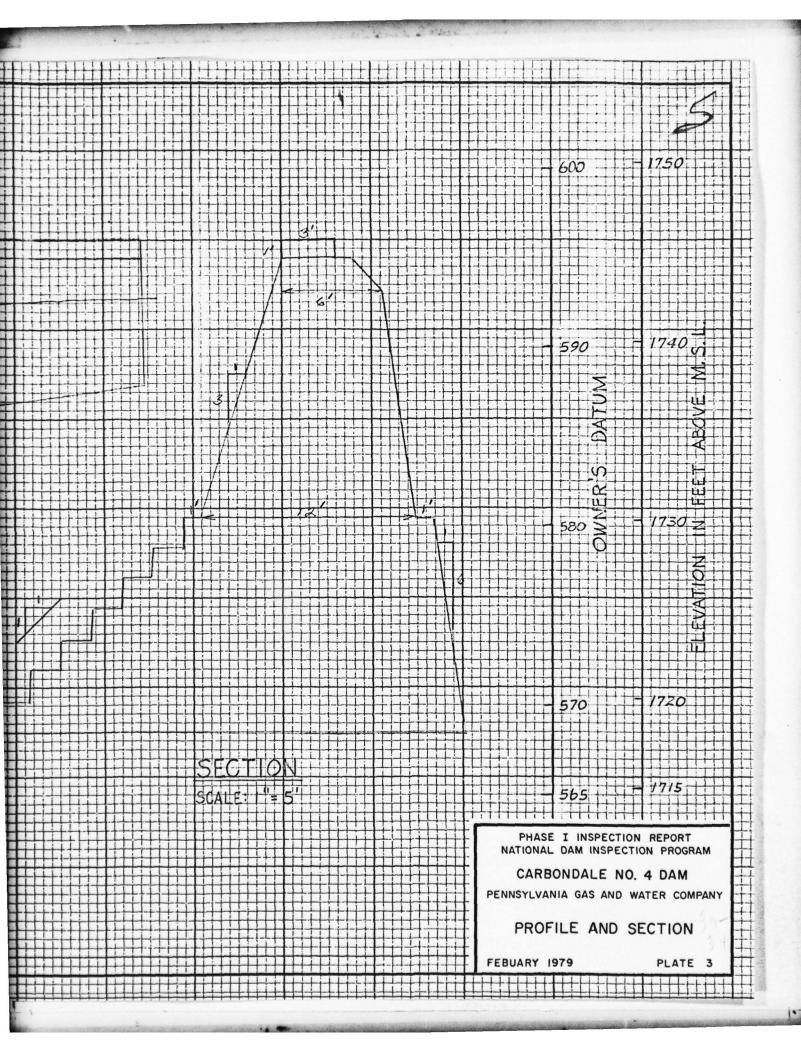


PROFILE

HORIZ. SCALE: II = 20 

NOTE:
Traced From
Penn Der File Dated
C. A. Wright - Enginee





SCALES 1".10" Ory Well to be built CARBONDALE No. 4 DAM (AS Rebuilt in 1945+1946) PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM CARBONDALE NO. 4 DAM PENNSYLVANIA GAS AND WATER COMPANY SPILLWAY AND OUTLET WORKS FEBUARY 1979 PLATE 4

## SUSQUEHANNA RIVER BASIN RACKET BROOK, LACKAWANNA COUNTY PENNSYLVANIA

CARBONDALE NO. 4 DAM

NDI ID No. PA-00384 DER ID No. 35-13

PENNSYLVANIA GAS AND WATER COMPANY

PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM

FEBRUARY 1979

APPENDIX A

CHECKLIST - ENGINEERING DATA

CHECKLIST

ENGINEERING DATA

DESIGN, CONSTRUCTION, AND OPERATION PHASE I

NAME OF DAM: CARBONDALE NO. 4
NDS ID NO.: DER ID NO.: 35-13

Sheet 1 of 4

ITEM	REMARKS
AS-BUILT DRAWINGS	PROFILE AND SECTION OF MASONRY PLATE 2
REGIONAL VICINITY MAP	SEE PLATE 1
CONSTRUCTION HISTORY	Buict 1892 Spiriumy Modified 1945
TYPICAL SECTIONS OF DAM	SEE PLATE 2
OUTLETS: Plan Details Constraints Discharge Ratings	NONE AVAILABLE

-	LA	5
-		2
-	Ö	ξ
	L	1
-	C	5
	L	i

Sheet 2 of 4

MEN	REMARKS
RAINFALL/RESERVOIR RECORDS	Now F
DESIGN REPORTS	None
GEOLOGY REPORTS	Nov F
DESIGN COMPUTATIONS: Hydrology and Hydraulics Dam Stability Seepage Studies	NONE
MATERIALS INVESTIGATIONS: Boring Records Laboratory Field	None
POSTCONSTRUCTION SURVEYS OF DAM	No. Kr

NONE

Sheet 3 of 4

ENGINEERING DATA

ITEM	REMARKS
BORROW SOURCES	NOT ALALLABLE
MONITORING SYSTEMS	None
MODIFICATIONS	PRESENT SPILLMMY CONSTRUCTED IN 1945
HIGH POOL RECORDS	JUNE, 1942 OVERTOPPED SLIGHTLY PEAK OUTFLOW = 200CFS
POSTCONSTRUCTION ENGINEERING STUDIES AND REPORTS	1914 PENNSYLVANIA WATER SUPPLY Commission Report
PRIOR ACCIDENTS OR FAILURE OF DAM: Description Reports	ROAD BELOW CHAN WAS WASHED OUT,

ENGINEERING DATA

Sheet 4 of 4

ITEM	REMARKS
MAINTENANCE AND OPERATION RECORDS	NOT AVALLABLE
SPILLWAY: Plan Sections Details	
OPERATING EQUIPMENT: Plans Details	NOT AVAILABLE
PREVIOUS INSPECTIONS Dates Deficiencies	1919- SEEPAGE THROUGH MASONRY JOINTS AND UNDER DAM AT DOWNSTREAM TOE. Spill WAY JOINTS NEED REPAIR 1924- Spill WAY ABUTMENTS HAVE MINOR SETTLEMENT, SMALL AMOUNT OF SEEPAGE TO LEFT OF OUTLET. POINTING NEEDED. 1928- SMALL FLOW TO LEFT OF OUTLET PIPE.
(continued)	1932 - Some SEEPHEET THROUGH MASONAY. 1941 - Joint S NEED REPOINTING. SLIENT FLOW UNDER OUTLET DIPE AND SLIENT FLOW IN TILE DRAIN.

Sheet 4a of 4

ENGINEERING DATA

REMARKS	THEOUGH TO THE	LOWER TOE DS FROT LEFT OF ORIGINAL HOUSE LEAKINGE IN TILE DERIN. 1953 - NO DEFICIENCES 1965 - NO DEFICIENCES		
ITEM	PREVIOUS INSPECTIONS (CONTINUED)			

## SUSQUEHANNA RIVER BASIN RACKET BROOK, LACKAWANNA COUNTY PENNSYLVANIA

### CARBONDALE NO. 4 DAM

NDI ID No. PA-00384 DER ID No. 35-13

PENNSYLVANIA GAS AND WATER COMPANY

PHASE I INSPECTION REPORT

NATIONAL DAM INSPECTION PROGRAM

FEBRUARY 1979

APPENDIX B

CHECKLIST - VISUAL INSPECTION

## CHECKLIST

0

# VISUAL INSPECTION

## PHASE I

NDS ID No.: 79-00384 DER ID No.: 35-13	Type of Dam: Masoney GRAVIN W/FILL UPSTREAM Hazard Category: HIGH  10/25 CLERA  Date(s) Inspection: October 25 4 26 1978 Weather: 19/26 RAIN  Contraction: October 25 4 26 1978 Weather: 19/26 RAIN  Contraction: October 25 4 26 1978 Weather: 19/26 RAIN		Pool Elevation at Time of Inspection: 1741, 4 msl/Tailwater at Time of Inspection: None msl	Inspection Personnel:  D. E besself (GFCL)  D. Wolf (GFCL)  J. Boomar (PCW)	A. WHITMAN (GFCC) Recorder
NDS I	Type o		Pool E	ag a a b	
		H.64	H16H	HiGH HiGH of Inspect	Hi6H Hi6H

GONGRETE/MASONRY DAMS

Sheet 1 of 2

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
ANY NOTICEABLE SEEPAGE	NONE	
JUNCTION OF STRUCTURE WITH:  Abutment Embankment Other Features	NO DEFICIENCIES	
DRAINS	None	
Water Passages	SEE OUTLET WORKS	
FOUNDATION	NOT VISIBLE	

GONGRETE/MASONRY DAMS

Sheet 2 of 2

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
M # SONRY GONGRETE SURFACES: Surface Cracks Spalling	NO DEFICIENCIES	
STRUCTURAL CRACKING	NONE	BURROWING ANIMAL HOLES DOWNSTREAM OF MASONRY.
ALIGNMENT: Vertical Horizontal	SEE PROFILE AND SECTIONS FOLLOWING INSPECTION FORMS	LOW AREA AT RIGHT ABUT MENT
MONOLITH JOINTS	M/A	
CONSTRUCTION JOINTS	MORTAR IS IN SENGRALLY GOOD CONDITION.	
STAFF GAGE OR RECORDER	None	

EMBANKMENT UPSTREAM OF MASONRY DAM

REMARKS OR RECOMMENDATIONS	ABUTHENT FMBANKMENT		
GOOD CONDITION	Sparse Except Negr LEFT ABUTMENT WHERE IT IS THICKER.		
VISUAL EXAMINATION OF RIPRAP	BRUSH		

OUTLET WORKS
Sheet 1 of 1

REMARKS OR RECOMMENDATIONS		SEEPACE IN STREAM OF O. 5 APM. MAY BE FROM NATURAL GROUND WATER.	NOT A HARARD.	NO DEFICIENCY.
OBSERVATIONS CAST IRON Pipe 2-36" DiA.	SUBMERGED	OUTFALL OF Pipes:	SLIGHTLY OVER BROWN WITH A FEW DEAD TREES.	VALVES 1 LINE OPENED ABOUT 5% by 2 men in 5 minutes
VISUAL EXAMINATION OF CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	INTAKE STRUCTURE	OUTLET STRUCTURE	OUTLET CHANNEL	EMERGENCY GATE

UNGATED SPILLWAY
Sheet 1 of 1

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
GONGRETE WEIR	MANY MINOR SEEPS THROUGH MASONRY JOINTS AND 1 MAJUR SEEP 6" DELOW CREST- 18PM	IN MASONRY TO RIGHT OF SPILLWAY, THE TOINTS ARE SEEPING.
APPROACH CHANNEL	RESERVOIR	
DISCHARGE CHANNEL	SEE SKETCH ON Next Sheet	
BRIDGE AND PIERS	None	

GANNETT FLEMING CORDDRY AND CARPENTER, INC. HARRISBURG, PA. SHEET NO. OF SHEETS

CONCRETE APRON RESERVOIR IN BEST CONDITION AT TOP OF SPILLWAY. SPALLING SPALLING APRON SCOURED Over 80% REBAR EXPOSED. SOME AREAS SCOURSO COMPLETES PATTERN CRACKING SPALLING ON FACE I BAFFLE BLOCK BY IS FT. LONG. SPALLED BADLY, REBAR EXPOSED FOTAL SEEPAGE ABOUT 28pm. ENTIRE SPALLING TOP HEAVY BRUSH SPALLED REBAR Exposed

Spillway OUTLET CHANNEL

INSTRUMENTATION
Sheet 1 of 1

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
MONUMENTATION/SURVEYS	None	
OBSERVATION WELLS	None	
WEIRS	2000	
PIEZOMETERS	NONG	
OTHER	NONE	

RESERVOIR AND WATERSHED

## Sheet 1 of 1

REMARKS OR RECOMMENDATIONS			ABITED CARBONDALE NO.7 DAM UPSTREAM	
OBSERVATIONS	IVON 2HI	NO REPORTED OR VISIBLE PROBLEMS.	WOODED AND UNINHABITED EXCEPT FOR A FEW MAINTENANCE BUILDINGS	
VISUAL EXAMINATION OF	SLOPES	SEDIMENTATION	WATERSHED DESCRIPTION	

DOWNSTREAM CHANNEL

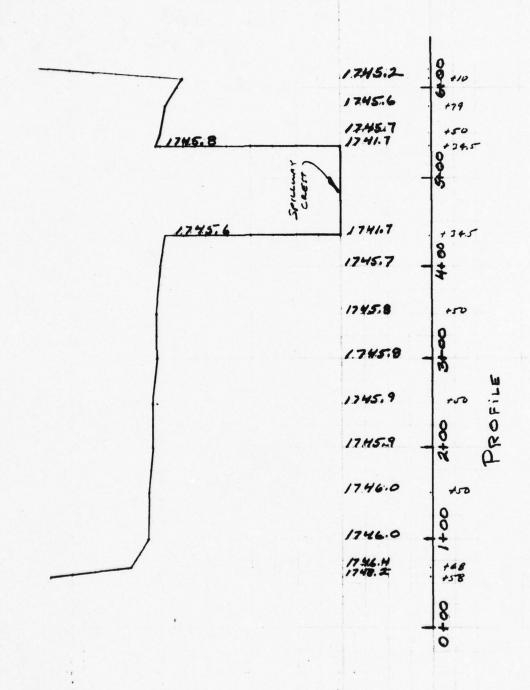
## Sheet 1 of 1

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONDITION: Obstructions Debris Other	PASSES UNDER U.S. ROUTE 6 - SEE SKETCH.	U.S. Route 6
SLOPES	Steep	
APPROXIMATE NUMBER OF HOMES AND POPULATION	NONE UNTIL BROWNELL DAM.	

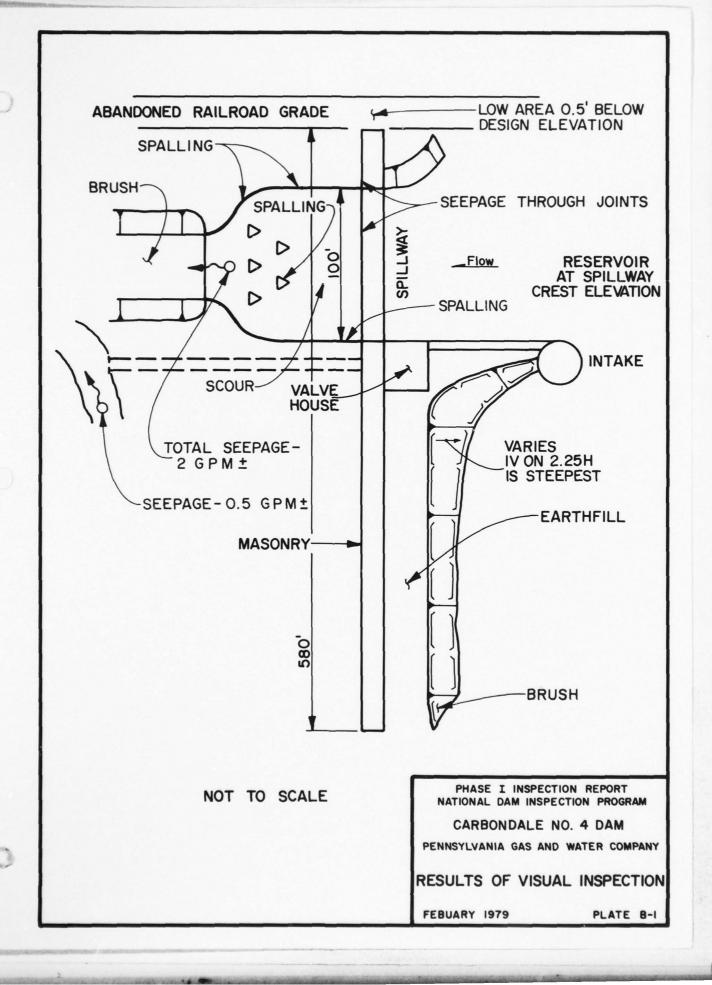
GANNETT FLEMING CORDDRY
AND CARPENTER, INC.
HARRISBURG, PA.

PAUFILE - TAP OF EMBANKMENT SHEET NO. OF SHEETS

FOR DATE 12-8-78 CHECKED BY DATE



SUBJECT CAKBONUALE NO 4 DAM GANNETT FLEMING CORDDRY SECTION - EMBANKMENT AND CARPENTER. INC. HARRISBURG. PA. COMPUTED BY DRE 5TA 4+18.5 1737.7 1737.7 1737.7 SCALE: 1"=10" 30 SECTIONS B-12



### SUSQUEHANNA RIVER BASIN RACKET BROOK, LACKAWANNA COUNTY PENNSYLVANIA

CARBONDALE NO. 4 DAM

NDI ID No. PA-00384 DER ID No. 35-13

PENNSYLVANIA GAS AND WATER COMPANY

PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM

FEBRUARY 1979

APPENDIX C
HYDROLOGY AND HYDRAULICS

### APPENDIX C

### HYDROLOGY AND HYDRAULICS

In the recommended Guidelines for Safety Inspection of Dams, the Department of the Army, Office of the Chief of Engineers (OCE), established criteria for rating the capacity of spillways. The recommended Spillway Design Flood (SDF) for the size (small, intermediate, or large) and hazard potential (low, significant, or high) classification of a dam is selected in accordance with the criteria. The SDF for those dams in the high hazard category varies between one-half of the Probable Maximum Flood (PMF) and the PMF. If the dam and spillway are not capable of passing the SDF without overtopping failure, the spillway capacity is rated as inadequate. If the dam and spillway are capable of passing one-half of the PMF without overtopping failure, or if the dam is not in the high hazard category, the spillway capacity is not rated as seriously inadequate. A spillway capacity is rated as seriously inadequate if all of the following conditions exist:

- (a) There is a high hazard to loss of life from large flows downstream of the dam.
- (b) Dam failure resulting from overtopping would significantly increase the hazard to loss of life downstream from the dam from that which would exist just before overtopping failure.
- (c) The dam and spillway are not capable of passing one-half of the PMF without overtopping failure.

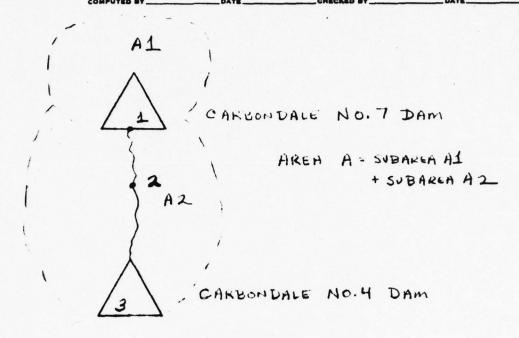
### APPENDIX C

	SUSQUE	Amonh	Riv	er Basin
Name	of Stream:	Koc	KET BROOK	
Name	of Dam: _	CARE	ON STHUMO	.4
NDS	ID No.:	PA-0	0384	
DER	ID No.:	35-13		
		0"	Longitude: W	75° 27' 35"
Top of Dam (lo	w opet) Elev	vation: _	1745.7	
Streambed Elev	ation: 17	17.7*	Height of Dam:	ft
Reservoir Stora	ge at Top o	f Dam Ele	vation:	o7/ acre-ft
Size Category:	INI	KMEUIA	ITE	
Hazard Catego	ry: H.G.	н		(see Section 5)
Spillway Desig				ROWNELL DAM
# FF	011		M DAMS	SDF : PMF
TO OUTLES WOR	Distance		Storage	
Name	from Dam (miles)		at top of Dam Elevation (acre-ft)	Remarks
CHREDNOHLEN	10.7 0.6	11	157	DER DATA (DER ID 64-1)
				( ) ( )
		-		
	Ī	OOWNSTR	EAM DAMS	
BROWNELL	0.70	64	2,995	FROM PHASE I
				Report

SUSQUEHA	AMIL	_ River Bas	in
Name of Stream: R	ACKET BRO	OOK	
Name of Dam:	BONDALE	NO.4	_
NDS ID No.: PA-	18500		
DER ID No.: 35-	13		
Latitude: N 41° 34' 30	Longitude	W 75	° 27' 35"
<u>DETERM INATIO</u>	N OF PMF RAI	NFALL	
For Area A			-
which consists of Subareas	A1 of	0.28	sq. mile
-	A2	1.40	
Total Drag	nage Area	1.68	sg. mile
PMF Rainfall Index =			
	(Susquehanna	Basin) (	Mydromet. 33 Other Basins)
Zone	N/A	-	
Geographic Adjustment Factor	95	%	1.0
Revised Index Rainfall	21.0		
RAINFALL DIST	RIBUTION (pe	rcent)	
Time	Percer	nt .	
6 hours	118	-	
12 hours 24 hours	<u> 127</u> <u> 136</u>	_	
48 hours			
72 hours	145		
96 hours	NIA	L	
	2-3		

GANNETT FLEMING CORDDRY
AND CARPENTER, INC.
HARRISBURG, PA.

SUBJECT	 	PILE NO.		
	 	SHEET NO	OF	SHEETS
FOR	 			



SKETCH OF SYSTEM

Data for Dam at Outlet of Subarea (see Sketch on Sheet C-4)	A-1	
Name of Dam: CARROLLAGE	No. 7	_ Sheet 1 of
Height:	(existing) OUTLE	T WORKS
Spillway Data:	Existing FLOOL	Design Conditions
Top of Dam Elevation	1813	ASSUMEO
Spillway Crest Elevation	1810	THE SAME
Spillway Head Available (ft)	3	
Type Spillway	SHARD CRESTED	WeiR
"C" Value - Spillway	3.1	
Crest Length - Spillway (ft)	29.8	
Spillway Peak Discharge (cfs)	480	
Auxiliary Spillway Crest Elevation	NONE	
Auxiliary Spillway Head Available	(ft)	
Type Auxiliary Spillway		
"C" Value - Auxiliary Spillway	-	
Crest Length - Auxiliary Spillway	(ft)	
Auxiliary Spillway Peak Discharge (	cfs)	
Combined Spillway Discharge (cf	s) <u>480</u>	
Spillway Rating Curve:		
Elevation O Spillway (cfs) OAu	xiliary Spillway (cfs)	Combined (cfs)
		THE RESERVE THE PARTY OF THE PA

Name of Dam: CAKBONDALE NO. 7 Sheet 3 of						
Storage Data: Storage						
Elevation	Area (acres)	million	acre-ft	Remarks		
1795.7 = ELEVO*	0	0	0			
1810 = ELEVI	20 = A1	31	95.1 = \$1	ASSUMED ELEV		
1813	21.4		157.3			
1820	25					
	-					
* ELEVO = ELEVI	- (3S <sub>1</sub> /A <sub>1</sub> )					
** Planimetered	ontour at leas	t 10 feet	above top of	iam		
Reservoir Area	Normal Pool at Top of Dan	is //	percent of	watershed.		
Remarks:						

C-6

Data for Dam at Outlet of Subarea <u>A1</u>

SUSQUEHOUTH River Basin
Name of Stream: RACKET TOROCK
Name of Dam: CAKBONDALE NO. 4
NDS ID No.: PA - 00384
DER ID No.: 35-13
Latitude: N 41° 34' 30" Longitude: W 75° 27' 35"
Drainage Area: 1.68 sq. mile
Data for Subarea: A1 (see Sketch on Sheet C-4)
Name of Dam at Outlet of Subarea: CARBONDALE NO.7
Drainage Area of Subarea: 0.28 sq. mile
Subarea Characteristics:
Assumed Losses: 1.0-inch initial abstraction + 0.05 in/hr
The following are measured from outlet of subarea to the point noted:
L = Length of Main Watercourse extended to the divide = $0.76$ mile
LCA = Length of Main Watercourse to the centroid = 0.23 mile
From NAB Data: ALLA 11, PLATE E
Cp = 0.62
$C_{T} = 1.50$
$Tp = C_T \times (L \times L_{CA})^{0.3} = \underline{O.89}  (hrs)$
Flow at Start of Storm = 1.5 cfs/sq. mile x Subarea D.A = 0.4 cfs
Computer Data:
QRCSN = $-0.05$ (5% of peak flow)
RTIOR = 2.0
Remarks:

Data for Dam at Outlet of Subarea <u>A-2</u> (see Sketch on Sheet C- <u>4</u> )					
Name of Dam: CARBONDALE	NO.4	Sheet 1 of			
Height: 28	( <del>onisting)</del>				
Spillway Data:	Existing Conditions	Design Conditions			
Top of Dam Elevation	1745.2	1745.7			
Spillway Crest Elevation	1741.7	1741.7			
Spillway Head Available (ft)	3.5	4.0			
Type Spillway	ROUNDED TOP				
"C" Value - Spillway	3.66*	3.66*			
Crest Length - Spillway (ft)	100.0	100.0			
Spillway Peak Discharge (cfs)	2396.5	2928			
Auxiliary Spillway Crest Elevation	NONE	NONE			
Auxiliary Spillway Head Available	(ft)				
Type Auxiliary Spillway					
"C" Value - Auxiliary Spillway					
Crest Length - Auxiliary Spillway	(ft)				
Auxiliary Spillway Peak Discharge (c	ofs)				
Combined Spillway Discharge (cfs					
Spillway Rating Curve: * From	LER REPORT, J	TUNE 1945			
Elevation O Spillway (cfs) OAu	xiliary Spillway (cfs)	Combined (cfs)			

Data for Dam at Outlet of Subarea	A-2	2
Name of Dam:CARRONDAL	. NO.4	Sheet 2 of
Outlet Works Rating:	Outlet 1	24" Ref 36" 36" Outlet 2 Outlet 3
Invert of Outlet	1717	
Invert of Inlet	NOT AVA	4.LABLE
Туре	CIP	
Diameter (ft) = D	3 24" DIAM.	
Length (ft) = L 60' -	36" DIAM.	
	- 3.14 - <u>T.07</u>	
N	.014**	
K Entrance	0.5	2.53 = K1
K Exit TRANSITION LOSS		47=K2 1.0 = K4
4 1/2	2.80	14.20 K3 .502=K
Sum of K		EKi = 18.702
$(1/K)^{0.5} = C$		0.23
Maximum Head (ft) = HM		28.7
$Q = C A \sqrt{2g(HM)} (cfs)$		69.9
Q Combined (cfs)		~ ~ 70
* FRONT CHOW	Losees i	N 24" SECTION WITH VELOCITIES (A) ON: KAYREF36= K24 (A)

<sup>\*</sup> R = Hydraulic Radius = (Area/Wetted Perimeter) = D/4 for Circular Conduits.

Data for Dam at Out	let of Subarea		12			
Name of Dam:	CHKBON	OHLE	NO.4	Sheet 3 of		
Storage Data:	Area	million	age	•		
Elevation	(acres)	gals	acre-ft	Remarks		
1702.5 = ELEVO*	0	0	0			
1741.7 = ELEVI	62 = A1	264	810.2 = S1			
1760 **	93					
**						
* ELEVO = ELEVI	- (3s <sub>1</sub> /A <sub>1</sub> )					
** Planimetered c	ontour at leas	t 10 feet	above top of d	lam		
Reservoir Area at Pop of Dem is						

SUSQUE HANNA River Basin
Name of Stream: RACKET BROOK
Name of Dam: CARBONDALE NO. 4
NDS ID No.: PA - 00384
DER ID No.: 35-13
Latitude: N 41° 34' 30" Longitude: W 75° 27' 35"
Drainage Area: 1.68 sq. mile
Data for Subarea: A-2 (see Sketch on Sheet C-4)
Name of Dam at Outlet of Subarea: CARBONDALE No. 4
Drainage Area of Subarea: /.4 sq. mile
Subarea Characteristics:
Assumed Losses: 1.0-inch initial abstraction + 0.05 in/hr
The following are measured from outlet of subarea to the point noted:
L = Length of Main Watercourse extended to the divide = $\frac{1.93}{1.93}$ mile
LCA = Length of Main Watercourse to the centroid = 0.65 mile
From NAB Data: AREA II, PLATE E
Cp = 0.62
$C_{T} = 1.50$
$Tp = C_T \times (L \times L_{CA})^{0.3} = /.6/$ (hrs)
Flow at Start of Storm = 1.5 cfs/sq. mile x Subarea D.A = 2.1 cfs
Computer Data:
QRCSN = $-0.05$ (5% of peak flow)
RTIOR = 2.0
Remarks:

### APPENDIX C

### SUMMARY

SEE SHEET C4		A2 Subarea			
Drainage Area (sq. mile)	0,28	THE THE			1.68
PMF:					
Peak Outflow (cfs)	925	4577			
Total Runoff (inches)					
Dam at Outlet?	YES	YES			
Is Dam Overtopped?	YES	YES			
Depth of Overtopping (ft)	0.66	1.31			
One-Half PMF:					
Peak Outflow (cfs)	362	2023			
Total Runoff (inches)					
Dam at Outlet?	YES	YES			
Is Dam Overtopped?	NO	NO			
Depth of Overtopping (ft)					
Does Dam Fail?	No	NO			
Peak Failure Outflow (cfs)					
At time (hrs)					-
Spillway (percent of PMF)	66	59			
DOW	NSTREAM	SUMMAR	X		
	Peak Wa Before F	ter Surfac	e Elevati Rer Failu	on re Re	marks
Cross Section	NOT	USEI	2		
Cross Section	-				
Cross Section					
Cross Section					
Cross Section					
	C-1	12			

GANNETT FLEMING CORDDRY AND CARPENTER, INC.	everet		SHEET NO. OF SHEETS
HARRIGBURG, PA.	COMPUTED BY DATE	CHECKED BY	DATE
	SELECTED Co	MPUTER COT	PuT
ITEM		Pac	F No.
INPUT		C-11	
System	PEAK FLOWS	C-	15
Summa	ey of Dams:		
C	ARBONDALE NO.	7 C	-16
		11	, -

300 0 15 0 0 -4  300 0 15 0 0 0 -4  1	٥		÷		1780	20•	
300 0 15 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7				950		
TOWER THEOLER NO. 4 DAN RACKET BROOK FIGURE NO. 7 TOWN STREET STATES FIGURE NO. 7 TOWN STA	•		<b>6</b>	•	1780	• 00	0
TOWER THROUGH NO. 4 DAN RACKET BROOK FIGURE 15 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	-	3	1810	420	245	4741.7 430 4750.0
CARBONDALE NO. 4 D  RACKET BROOK  SOC		٤.	162		1100 1800 1840	142	
CARBONDALE RACKET  SOO 0 15 6FCC  SOO 0 15 06  RUNDF INTO NO.7  ROUTE THROUGH NO.7  1 20 26  1813 2-7  1813 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 2-7  1815 125  1815 2-7  1815 125  1815 2-7  1815 125  1815 2-7  1815 125  1815 2-7  1815 125  1815 2-7  1815 125  1815 125  1815 2-7  1815 125  181	NO. 4 D	:	136		1800 290 1330	136	
300 0 15  5 6 6 6  1 9 6 6 6  1 1 0 8 6  1 1 0 8 6  1 1 10 8  89 662  190 662  1813 267 165  1813 267 165  1813 267 165  1813 267 165  1813 267 165  1813 267 165  1814 0 182  1815 267 169  1815 267 169  1816 0 1800 1180  1916 1 662  1917 1 161  1918 0 1000  1018 1	RACKET B	s.	127	1 200			
300 300 50 10 10 10 10 10 10 10 10 10 1	CAF 15		118	25 1820 3 1 1 0 5	.09 190 1180	104 118 2 2 NO.7819	
300 300 50 11 11 18 19 10 10 10 10 10 10 10 10 10 10			21 . - 62 - 05	20 1810 29.8 2.7 2.7 2.7	.07 1840 1800 3	21 262 -05 181 NE DUT	3 JTE THROU 1741.7 100 2.7 3.0 1745.6
*		2 - 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -	. 89 -1-5	1 0 1795.7 1810 1813	760	1.61	1702.5 1741.7 1745.2

FLOOD HYJROGRAPH FACKAGE (HEC-1)
DAW SAFETY VERSION
LAST MODIFICATION
11 JAN 79
RECEMBERS OF SERVICE S

C-14

FLAN FLOW AND STOKACE (EAD OF PLATOR) SUMMANY FOR MULTIPLE PLAN-SATIO FCONDHIC COMPUTATIONS FLOW AND STOKES FER SECOND (CURIC METERS PER SECOND) AREA IN SQUARE MILES (SQUARE KILCMETERS)

OPFEATION	STATION	AREA	FLAN	1.00 1 1.00	FAT10 2	RATIOS APPLIED TO FLUES FLAM KATIO 1 FATIO 2 FATIO 3 FATIO 5 FATIO 5 1.60 .80 .60 .50 .40 .30	RATIO 4 *50	245 5 6116 5	6. STIC 6.30
HYDEGGRAPH AT	_~	.733	-~	1053.	942.	17.8916	14.9030		316.
30UTED TO	_~	•29	-~	925.	19.37)	12,5730		243.	5.7936
ROUTED TO	~~	•28	-~	931.					
HYDROCRAPH AT	~~	1.40	-~	3956.	3165.		1978.		
2 COMBINED	~~	1.68	-~	136.95)(	3841.	2816.			
ROUTED TO	<b>.</b> ~	1.68		4577.					

SUMMARY OF THE TREETY SHALVSES

. 1 10

		TIME OF FAILURE HOURS	000000		
AM	1615.00 1615.00 157. 480.	TIME OF MAY OUTFLOW HOURS	41.00 41.25 41.50 41.50 61.50		
2	=	DURATION OVER TOP HOURS	2.7.7.0 0.00 0.00 0.00 0.00 0.00 0.00	7 TIME MOURS	1, 200
ALE N	18.6.03 18.10.60 18.15.90 18.5.00 18.15.90 18.7.00 18.	HAKIMUM OUTFLOW CFS	925. 684. 464. 362. 253. 293.	STATION MAXIMUM STAGE SFT	1780.9 1786.6 1786.6 1780.3 1780.3
ARBOND	98.	MAXINUM STORAGE AC-FT	172. 165. 154. 147. 139.	PLAN 1 MAXIMUM FLOWACFS	931. 678. 444. 363. 283. 204.
O	1916-03 95•	DEFTH OVER DAN	000000000000000000000000000000000000000	PL RATIO	1.00 0.00 0.00 0.00 0.00 0.00
	ELCVATION STORAGE DUTFLOW	MAKIMUM RESEFVOIR V.S.ELEV	1813.006 1813.006 1812.65 1812.65 1812.11		
		64710 90 9 9	5.000000		

SUMMARY OF DAM CAFETY ANALYST

NATIO MAXIMUM MAXIMUM MAXIMUM PAXIMUM DE PER SENDIR DEPTM STOKAGE OUTFLOW PMS DAM AC-FT CFS 1600 1746-51 1-31 1126- 4577-60 1745-03 -06 1041- 2463-		STOFAGE	9	110. 0.	1741.70	15	37 45 20 1765 20 1057 - 2397 -	
174.5.51 1.31 1126. 174.5.03 .83 1093. 174.5.26 .06 1041.	SATIO OF PHF	PESENVOIR No Soft EV	MAKINUM DEPIN OVER DAM	STOKAGE AC-FT	HAXIMUM OUTFLOV CFS	DURATION OVER TOP HOUES	TIME OF MAX DUTFLOW HOURS	TIME OF
1745.26 .06 1041.	300	1746.51	1.31	1126.	4577	27.25	41.50	00.00
1744.83 0.00 1011.	900	1745.26	900	1041	2463	27.0	75.00	
1744.36 0.00 981. 1743.86 0.00 948.	.30	1744.36	0000	981.	1586.	0000	12.25	000

GANNETT	FLEMING	CORDDRY
AND C	ARPENTER	R. INC.
HA	RRISSURG.	PA.

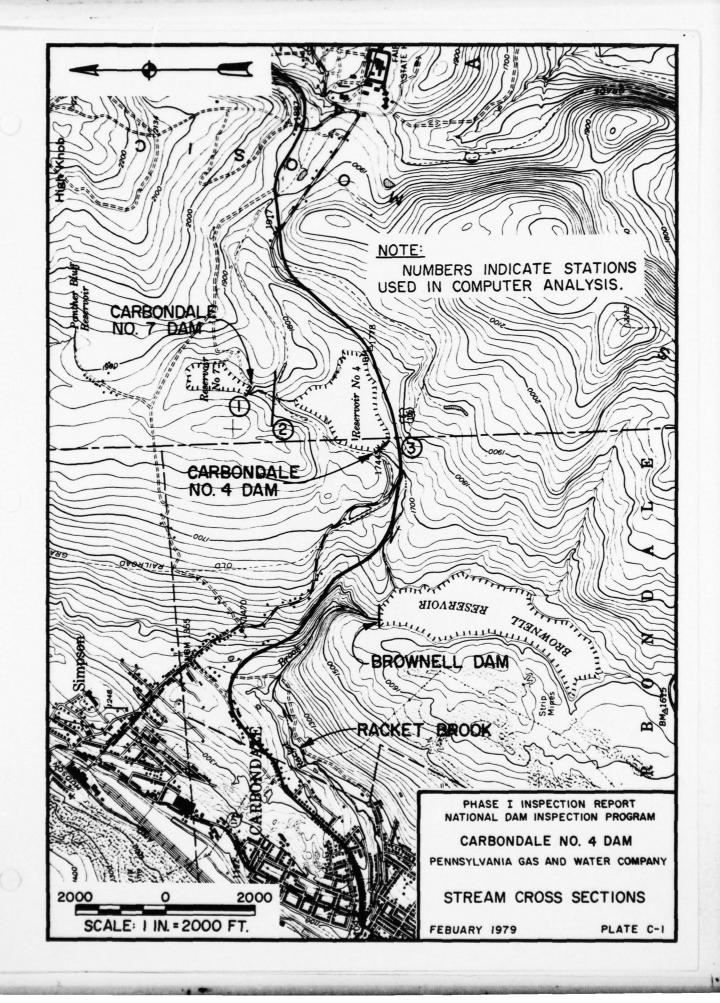
UBJECT			FILE HO		
			SHEET NO	OF	SHEETS
POR					
	2472	CHECKED BY	DAT		

SUMMARY OF RESULTS

(DAM WITH EXISTING CONDITIONS)

PMF RAINFALL = 24.4"

PITT RAINE	1966 = X7.4	
	PMF	1/2 PMF
RUNDER (INCHES)	22.0	11.0
PEAK INFLOW TO  CARBONDALE NO. 4 (CFS)	4,936	2,338
PEAK OUTFLOW FROM CARBONDALE NO.4 (CPE)	4,577	2,023
DEPTH OF OVERTOPPING OF CHEBONDAUE NO.4 (FT.)	1.31	_



## SUSQUEHANNA RIVER BASIN RACKET BROOK, LACKAWANNA COUNTY PENNSYLVANIA

CARBONDALE NO. 4 DAM

NDI ID No. PA-00384 DER ID No. 35-13

PENNSYLVANIA GAS AND WATER COMPANY

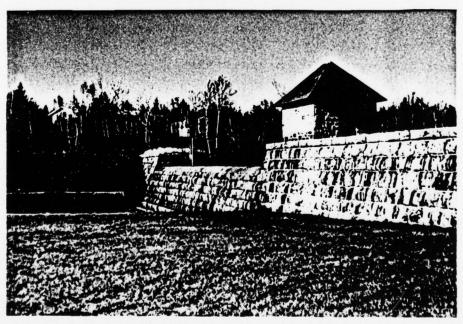
PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM

FEBRUARY 1979

APPENDIX D
PHOTOGRAPHS



A. Upstream Slope



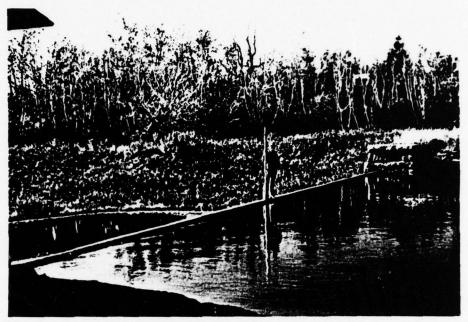
B. Downstream Face and Spillway



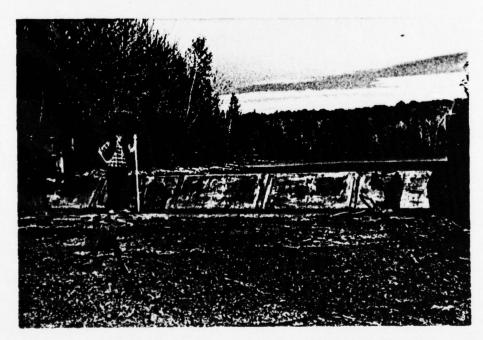
C. Spillway



D. Spillway Outlet Channel



E. Spillway Approach Channel



F. Spillway at Carbondale No. 7 Dam Upstream of Carbondale No. 4 Dam

# SUSQUEHANNA RIVER BASIN RACKET BROOK, LACKAWANNA COUNTY PENNSYLVANIA

### CARBONDALE NO. 4 DAM

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APPENDIX E
GEOLOGY

### APPENDIX E

#### **GEOLOGY**

1. General Geology. The damsite and reservoir are located in Lackawanna County. Lackawanna County was completely covered with ice during the last continental glaciation of Pleistocene time. The general direction of ice movement was S 35° - 40° W. Glacial drift covers the entire County, except where subsequent erosion has removed it. Thick deposits of glacial outwash occur in many places along the Lackawanna River, and are 50 to 100 feet thick near Dickson, Scranton, and Moosic.

The only important structural feature in Lackawanna County is the Lackawanna Syncline, which traverses the County in a southwesterly direction. syncline enters the County at the northeast corner as a narrow shallow trough, gradually deepens and broadens toward the southwest, and reaches its maximum development in Luzerne County. The rock formations exposed range from the post-Pottsville formations (youngest) through the Pottsville, Mauch Chunk shale, Pocono sandstone to the Damascus formation of the Catskill group (oldest). rim rocks, the Pottsville formation and Pocono sandstone, have dips that rarely exceed 10 to 20 and form a rather simple syncline. The core rocks, the post-Pottsville formations, are folded into a series of minor anticlines and synclines which trend about N 70° E. The rocks in the northwestern and southeastern parts of the County, outside of the limits of the Lackawanna Syncline, are generally horizontally stratified.

The Lackawanna River, in general, follows the axis of the Lackawanna Syncline. Southeast of the Lackawanna River, the rise in terrain is quite gradual and the crests of the high mountains are several miles from the Lackawanna River. Streams, such as Roaring Brook, Stafford Meadow Brook, and Spring Brook, have cut deep canyons through the mountains and follow a torturous course to their confluence with the Lackawanna River near Scranton, Pennsylvania. Northwest of Lackawanna River, the mountains rise abruptly to a sharp ridge which in most places is

somewhat higher than the country to the northwest. Consequently, most of the drainage in this part of the County flows westward by way of Tunkhannock Creek. A few small tributary streams, however, such as Leggetts Creek, flow eastward from this area into Lackawanna River. In the area of interest, the Lackawanna River streambed is founded in post-Pottsville formations. Proceeding uphill from the river, the older Pottsville formation, Mauch Chunk shale, Pocono sandstone, and Catskill continental group are encountered in turn. The tributary streams, in flowing down the mountains, have generally cut through or around the hard sandstone and conglomerate members, and have eroded their streambed into the softer shales and glacial till. The Catskill continental group of rocks underlies the greater part of Lackawanna County.

Site Geology. The damsite is located in the extreme northeast section of Lackawanna County while the reservoir is bisected by the Lackawanna/Wayne County line which runs north south. Carbondale No. 4 Dam is founded on the Catskill sandstones and siltstones of late Devonian The Catskill formation is composed of dark red shale, claystone, and siltstone; gray and dark red, fine to medium grained sandstone; and green, medium to coarse grained conglomerates. Crossbedding, channeling, and cut-and-fill features are common to the sandstone and conglomerate units. About half of the formation that is exposed in this area is composed of sandstone and coarser grained rocks, and the other half is composed of finer grained rocks. Siltstone predominates in the lower part of the formation. The rocks in this area are systematically jointed with two markedly preferred orientations. The prominent set in this area trends N 10 E. Bedding in this area is usually well developed with thicknesses ranging from 1 foot to 10 to 16 feet in the coarser, more competent beds.

The available records did not yield information pertinent to the foundation conditions at the damsite.

